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(58) Field of Search

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## (54) Method for identifying causes of faults in amperometric measuring cells

(57) The method identifies causes of faults in an amperometric measuring cell 1 which has at least an measuring electrode 2 and a counterelectrode 3 in a chamber 4 filled with a soluble electrolyte 6, and separated from the measurement sample being investigated by a permeable membrane 7, and a voltage source 10 of potential  $U$ , which produces a reference current  $i(t)$  between the electrodes 2, 3. The potential  $U$  is raised or lowered to a first potential  $U_1$  during a first period of time  $T_1$ , and the resulting first sensor current  $i_1$  is measured and compared with the reference current. The first sensor current may be measured shortly after the adjustment to the first potential  $U_1$ , or towards the end of the first period of time  $T_1$ . During a second period, following the first period  $T_1$ , the potential may be adjusted to a second potential which is less than  $U$  if  $U_1$  was greater than  $U$ , or greater than  $U$  if  $U_1$  was less than  $U$ .

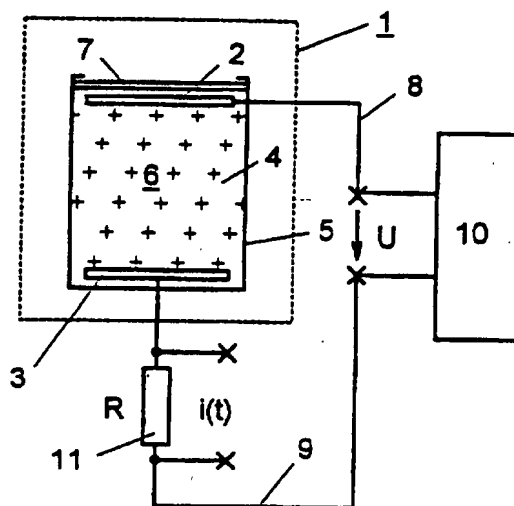


Fig.1

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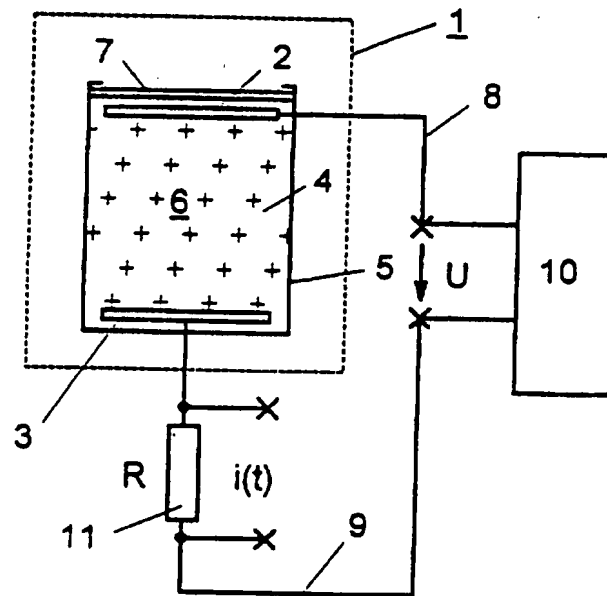


Fig.1

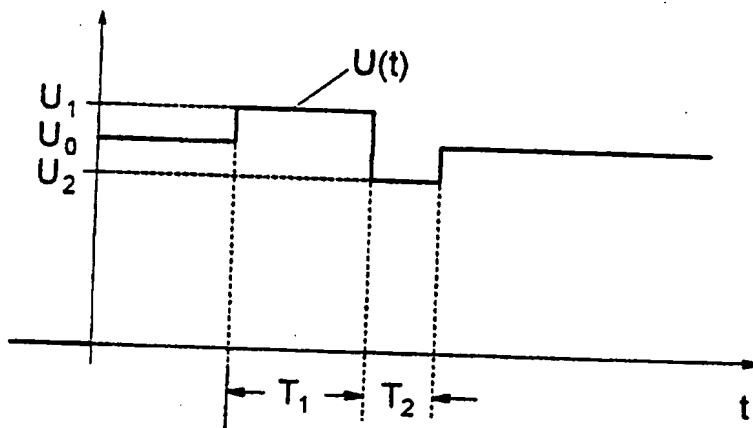
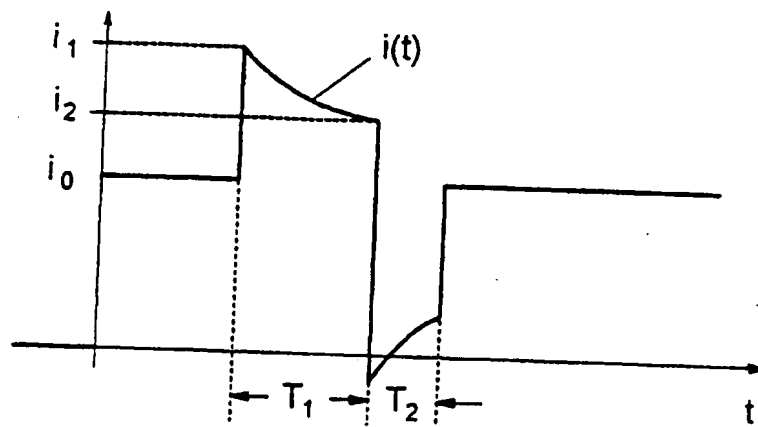


Fig. 2

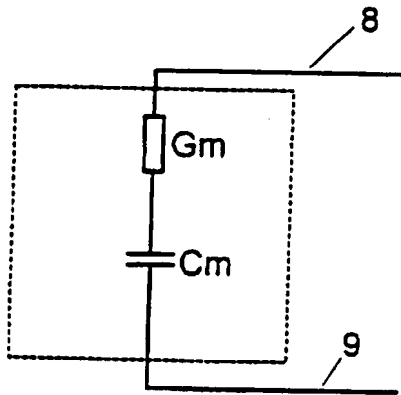


Fig. 3

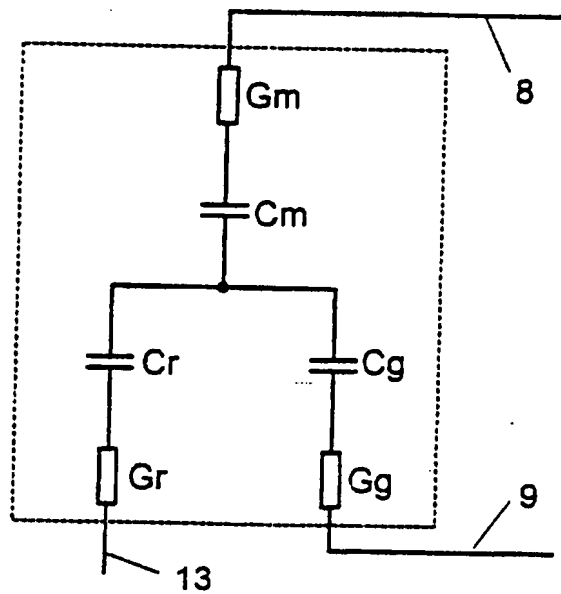


Fig. 4

METHOD FOR IDENTIFYING CAUSES OF FAULTS IN AMPEROMETRIC MEASURING CELLS

The invention relates to a method for identifying causes of faults in an amperometric measuring cell  
5 which has at least a measuring electrode and a counterelectrode in an electrolyte-filled electrolyte chamber, separated from the measuring sample being investigated by a permeable membrane, and which is connected to a voltage source which produces a sensor  
10 current between the electrodes and provides a potential.

An electrochemical measuring cell of this kind has been disclosed in DE 38 41 622 C1. A measuring electrode, a reference electrode and a counterelectrode  
15 are fitted in an electrolyte-filled electrolyte chamber of a measuring cell housing which is separated from the sample being investigated by means of a permeable membrane. The measuring electrode, the reference electrode and the counterelectrode have measuring  
20 connections which are led out through the housing of the measuring cell and are connected to an evaluation unit having a voltage source. After connection of the electrodes to the voltage source a sensor current  $i(t)$  begins to flow.

25 It is a disadvantage of the known measuring cell that it is not possible to obtain any indication of the service condition of the measuring cell. Thus it may, for example, happen that although the sensor current  $i(t)$  falls within its predetermined limits, an accurate  
30 measurement of concentration is nevertheless no longer possible with the measuring cell.

From EP 419 769 A2 a method for continuous monitoring of an electrode system of potentiometric measuring cells is known in which symmetrical bipolar  
35 current pulses of different periods are repeatedly applied to the measuring cell and the change in

potential thereby produced, relative to the electrode potential without current pulses, is compared with a calculated or experimentally determined intended value.

This known process has the disadvantage that an additional voltage source is required by means of which the test is carried out, and that for the detection of the individual faults the test must be performed at different times and using different periods.

The present invention seeks to provide a process for the identification of the causes of faults for amperometric measuring cells by means of which different faults can be identified within one measuring cycle.

According to the present invention, there is provided a method for identifying causes of faults in an amperometric measuring cell which has at least one measuring electrode and a counterelectrode in a soluble electrolyte-filled electrolyte chamber separated from the measuring sample being investigated by a permeable membrane, and which is connected to a voltage source which produces a sensor current between the electrodes and provides a potential, the method comprising the steps of:

applying a reference potential and measuring a reference current flowing due to the application of the reference potential;

applying a first potential, different from the reference potential, during a first period of time and measuring a first sensor current flowing due to the application of the first potential; and

comparing the first sensor current with the reference current.

Thus, starting from a reference potential  $U_0$ , with a reference current  $i_0$ , a first potential  $U_1$  is applied during a first period of time  $T_1$  and a first sensor current  $i_1$  is measured shortly after the application of

the first potential  $U_1$ , and/or a second sensor current  $i_2$  is measured near the end of the first period of time  $T_1$ , and the sensor current  $i_1$  and/or  $i_2$  is compared with the reference current  $i_0$ .

5       The advantage of the invention is essentially that through a slight modification of the potential, i.e. by raising or lowering the potential to a first potential  $U_1$  during a first period of time  $T_1$ , a change in the sensor current  $i(t)$  from  $i_1$  to  $i_2$  is produced, and that  
10 the comparison of the first sensor current  $i_1$  and/or of the second sensor current  $i_2$  with the reference current  $i_0$  is used to detect a fault in the measuring cell. To perform this measurement only a slight modification of the potential, in the region of about 0.02 to 1  
15 millivolt, is required. The first period of time  $T_1$  amounts to about 100 milliseconds. If the method of the invention is carried out during the exposure of the measuring cell to the sample of gas to be investigated, the reference current  $i_0$  is the measuring current, and  
20 in a neutral gas atmosphere the stationary sensor base current forms the reference current.

The sub-claims are directed to advantageous embodiments of the invention.

Advantageously, during a period of time  $T_2$ ,  
25 following the first period of time  $T_1$  the potential is adjusted to a second potential  $U_2$  which, relative to the reference potential  $U_0$ , is directed oppositely to the first potential  $U_1$ . This results in reversal of polarity within the measuring cell, and after the end  
30 of the second period of time  $T_2$  the reference current  $i_0$  again flows in the measuring cell.

The length of the second period of time  $T_2$  is advantageously not more than 1.5 times the first period of time  $T_1$ .

35       The second period of time  $T_2$  is advantageously calculated by the formula

$$T_2 = T_1 \times \ln(1 - Y \times (1/X)) / \ln(X)$$

where

$$X = (i_1 - i_0) / (i_2 - i_0) \quad \text{and}$$

$$Y = (U_1 - U_0) / (U_2 - U_0).$$

5      Advantageously the parameters  $C_m$  and  $G_m$  characterising the measuring cells are calculated by the formulae:

$$G_m = (i_1 - i_0) / (U_1 - U_0)$$

$$C_m = T_1 \times G_m / \ln((i_1 - i_0) / (i_2 - i_0)).$$

10      The parameters  $C_m$  and  $G_m$  may, for example, be compared with predetermined values  $C_{m0}$  and  $G_{m0}$ , an indication being given, if a previously established limiting value is exceeded, that the measuring cell is exhausted or damaged and must be exchanged for a new  
15 one.

For a better understanding of the present invention, and to show how it may be brought into effect, reference will now be made, by way of example, to the accompanying drawings, in which:

- 20      Fig. 1      shows schematically the design of an amperometric measuring cell with two electrodes,  
Fig. 2      shows how the sensor current varies with time on application of the potentials  $U_1$  and  $U_2$ ,  
25      Fig. 3      is an equivalent circuit diagram of the measuring cell of Fig. 1, and  
Fig. 4      is an equivalent circuit diagram of a measuring cell with an additional  
30      reference electrode.

Figure 1 shows schematically the design of an electrochemical measuring cell (1) having a measuring electrode (2) and a counterelectrode (3) which are fixed in an electrolyte chamber (4) of a measuring cell  
35 housing (5). The measuring cell housing (5) is filled with an electrolyte (6) in aqueous solution and is



separated from the gas sample to be investigated by a permeable membrane (7). The electrodes (2, 3) are connected by leads (8, 9) to a voltage source (10) by means of which a potential  $U$  is applied to the electrodes (2, 3). The sensor current  $i(t)$  is detected as a potential drop across a measuring resistance (11) in the lead (9).

Figure 2 shows the variation of the sensor current  $i(t)$  with time in dependence on the potential  $U(t)$ .

During a first period of time  $T_1$  the potential  $U$  is raised to the first potential  $U_1$ , so that the sensor current  $i(t)$  increases from the reference current  $i_0$  to the first sensor current  $i_1$  and then falls during the first period of time  $T_1$  to the second sensor current  $i_2$ .

During a second period of time  $T_2$  following the first period of time  $T_1$  the potential is lowered to the second potential  $U_2$ , and the sensor current  $i(t)$  falls relative to the reference current  $i_0$ , and after the second period of time  $T_2$  again assumes the reference current value  $i_0$ .

The sensor currents  $i_0$ ,  $i_1$  and  $i_2$  are read into an evaluation unit (not shown in Figure 1) which includes a microprocessor that compares the sensor currents and performs calculations. Through the evaluation unit the variations of the potential from  $U_0$  to  $U_1$  and from  $U_1$  to  $U_2$  or from  $U_2$  to  $U_0$  are also controlled. The first potential  $U_1$  is selected to lie about 0.02 to 1 mV above the reference potential  $U_0$ , and the length of the first period of time  $T_1$  is about 100 milliseconds. The length of the second period of time  $T_2$  is selected to amount to from about 0.2 to 1.5 times the first period of time  $T_1$ .

The second period of time  $T_2$  can also be calculated from the measured sensor currents  $i_0$ ,  $i_1$  and  $i_2$  on the basis of a simplified equivalent circuit diagram shown in Figure 3.

The measuring cell (1), Figure 1, can be

represented electrically by a measuring electrode capacitance  $C_m$ , which is made up of the measuring electrode (2) and the counterelectrode (3), with the electrolyte (6) situated between them, and a measuring electrode conductance  $G_m$ , which reflects the ohmic resistance between the electrodes (2, 3) and the contact resistances between the electrodes (2, 3) and the leads (8, 9).

The second period of time can be calculated from the formula

$$T_2 = T_1 \times \ln(1 - Y \times (1/X)) / \ln(X)$$

where

$$X = (i_1 - i_0) / (i_2 - i_0) \quad \text{and}$$

$$Y = (U_1 - U_0) / (U_2 - U_0).$$

The measuring electrode capacitance  $C_m$  and the measuring electrode conductance  $G_m$  are given by the calculation formulae:

$$G_m = (i_1 - i_0) / (U_1 - U_0)$$

$$C_m = T_1 \times G_m / \ln((i_1 - i_0) / (i_2 - i_0)).$$

In the evaluation unit predetermined values for the measuring electrode capacitance and the measuring electrode conductance are stored as reference measuring electrode capacitance  $C_{m0}$  and as reference measuring electrode conductance  $G_{m0}$ , and in the evaluation unit a comparison of the calculated parameters  $C_m$  and  $G_m$  with the predetermined values  $C_{m0}$  and  $G_{m0}$  is performed.

Deviations of the parameters  $C_m$ ,  $G_m$  from the preset values  $C_{m0}$ ,  $G_{m0}$  can have the following causes:

For example, faulty contact with the measuring electrode only affects the measuring electrode conductance  $G_m$ , while reduced wetting of the measuring electrode (e.g. due to drying out) shows up predominantly in the measuring electrode capacitance  $C_m$ . Since in addition the temperature dependence of  $G_m$  and  $C_m$  can readily be determined and moreover is approximately linear over a wide range, the possible

tolerance limits for  $C_m$  and  $G_m$  can be selected relatively narrowly. Consequently not only can a complete failure of the sensor be detected, but changes can already be recognised which would only lead to a failure later on, or which would have an unacceptable effect on the measuring properties of the sensor.

The method of the invention for the identification of faults can also be used in the same way for a three-electrode measuring cell (12) with a reference electrode, the equivalent circuit diagram of which is represented in Figure 4. Components in Figure 4 which are the same as in Figures 1 and 3 are indicated by the same reference numerals. The reference electrode, not shown in Figure 4, is connected to a lead (13). In the equivalent circuit diagram of Figure 4  $G_g$  is the counterelectrode capacitance,  $C_g$  is the counterelectrode capacitance,  $G_r$  is the reference electrode conductance, and  $C_r$  is the reference electrode capacitance. The conductances can be physically understood as resistance of the leads to the electrodes, contact resistance between lead and electrode and contact resistance between electrode and electrolyte, and the capacitances are double layer capacitances between the electrodes.

CLAIMS

1. A method for identifying causes of faults in an amperometric measuring cell which has at least one measuring electrode and a counterelectrode in a soluble electrolyte-filled electrolyte chamber separated from the measuring sample being investigated by a permeable membrane, and which is connected to a voltage source which produces a sensor current between the electrodes and provides a potential, the method comprising the steps of:
  - applying a reference potential and measuring a reference current flowing due to the application of the reference potential;
  - applying a first potential, different from the reference potential, during a first period of time and measuring a first sensor current flowing due to the application of the first potential; and
  - comparing the first sensor current with the reference current.
2. A method for identifying causes of faults in an amperometric measuring cell as claimed in claim 1, wherein the first sensor current is measured shortly after the beginning and/or shortly before the end of the first period.
3. A method according to claim 1 or 2, in which during a second period of time following the first period of time the potential is adjusted to a second potential which is greater than the reference potential if the first potential is less than the reference potential and is less than the reference potential if the first potential is greater than the reference potential.
4. A method according to claim 3, wherein the length of the second period of time is not more than 1.5 times the first period of time.
5. A method according to claim 3, wherein the

second period of time is calculated by the formula:

$$T_2 = T_1 \times \ln(1 - Y \times (1/X)) / \ln(X)$$

where

$T_1$  = first period of time

5  $T_2$  = second period of time

$$X = (i_1 - i_0) / (i_2 - i_0)$$

$$Y = (U_1 - U_0) / (U_2 - U_0)$$

$i_0$  = reference current

10  $i_1$  = sensor current shortly after start of first period

$i_2$  = sensor current shortly before end of first period

$U_0$  = reference potential

$U_1$  = first potential

15  $U_2$  = second potential.

6. A method according to one of claims 1 to 5, wherein the parameters  $C_m$  and  $G_m$  electrically representing the electrochemical measuring cell are calculated according to the formulae:

20  $G_m = (i_1 - i_0) / (U_1 - U_0)$

$$C_m = T_1 \times G_m / \ln((i_1 - i_0) / (i_2 - i_0)).$$

$T_1$  = first period of time

$i_0$  = reference current

25  $i_1$  = sensor current shortly after start of first period

$i_2$  = sensor current shortly before end of first period

$U_0$  = reference potential

$U_1$  = first potential.

30 7. A method according to claim 6, characterised in that the parameters  $C_m$  and  $G_m$  are compared with preset values  $C_{m0}$  and  $G_{m0}$  in order to determine a fault in an amperometric measuring cell.

8. A method for identifying causes of faults in  
35 an amperometric measuring cell substantially as herein described with reference to Figures 1-3 or 1, 2 and 4

-10-

of the accompanying drawings.



11  
**The  
Patent  
Office**

**Application No:** GB 9526143.4  
**Claims searched:** 1-8

**Examiner:** David Mobbs  
**Date of search:** 22 March 1996

**Patents Act 1977  
Search Report under Section 17**

**Databases searched:**

UK Patent Office collections, including GB, EP, WO & US patent specifications, in:

UK CI (Ed.O): G1N NBKT.

Int CI (Ed.6): G01N 27/416.

Other: NONE.

**Documents considered to be relevant:**

| Category | Identity of document and relevant passage | Relevant to claims |
|----------|---|--------------------|
| Y        | WO 94/08235 A1 FOXBORO                    | 1                  |
| Y        | WO 90/12315 A1 NEOTRONICS                 | 1                  |

|   |   |   |  |
|---|---|---|--|
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